

THE PROCESS FOR EXTRACTING GOLD IN ARSENIC-CONTAINING CONCENTRATE OF GOLD AND THE EQUIPMENT THEREOF

Technical Field

5 This invention concerns a method to extract gold from arsenic gold ore concentrate, especially concerns a method to extract fine grained gold from arsenic sulfide gold ore concentrate; this invention also concern a system to extract gold from arsenic gold ore concentrate.

10 Background Technology

To extract gold from the mineral, especially the fine grained and submicron gold in the pyrite, arsenopyrite ore and other sulfide ores, it must first completely remove arsenic in these minerals so as to effectively extract gold. It has been a big technical barrier in the gold production about how to completely remove the arsenic in the gold concentrate and also not to cause environment pollution, which has been restricting the gold output.

Conventional dearsenization method is to conduct oxidizing roasting of the arsenic gold ore concentrate or gold bearing arsenopyrite ore to oxidize the arsenic in the mineral into volatilized As_2O_3 and arrive at the purpose of dearsenization. Although this method is simple, it has four disadvantages: (1) In the roasting process, since some arsenic and gold generate a kind of low boiling point and volatilized arsenic and gold compound under the roasting temperature, about $900^{\circ}C$, thus greatly lowering the gold recovery. The gold loss percentage is often up to 25-35%. (2) It is hard to get qualified arsenic product. Since the Sb, Bi, Pb, Hg, Zn and other contaminating metals also volatilize and mix with As_2O_3 by form of oxides, As_2O_3 cannot meet the product requirement on purity and cannot be sold. To utilize the As_2O_3 byproduct, conventional method is

to put As_2O_3 into normal pressure electric heating vertical retort reducing furnace and use carbon to reduce As_2O_3 into element arsenic, involving heavy labor intensity. (3) Both oxidizing roasting process and the process reducing As_2O_3 into element As must deal with virulent As_2O_3 . Each operation link is hard to avoid environment pollution by As_2O_3 , especially even hard to assure the personal safety of operators. (4) It is not possible to remove arsenic. Since it is difficult to control the temperature of oxidizing roasting, some arsenic is left in the slag by form of oxide. Some arsenic turns into iron arsenate under high temperature and is left in the slag. The higher the temperature is, the higher arsenic content in the slag, which is not favorable for gold extraction in the next step.

To overcome the above disadvantages of using the As_2O_3 as raw material to produce element arsenic in the normal pressure reducing furnace, some research units made some small tests to directly extract element arsenic from arsenic concentrate by means of the vacuum process, such as the kilogram level test to remove arsenic from the cobalt ore in the existing technologies (China Non-ferrous Metal Journal, Book 4 Issue 1, 1993), which aimed at creating conditions for the next-step wet method extraction of element cobalt. The test theory was to enable thermal decomposition of the Co, Fe, Ni and As compound in the cobalt concentrate under vacuum conditions and separate out element arsenic. The experimental conditions were: residual pressure 6-10Pa and temperature 1100-1200 °C . But the experimental result had many problems: (1) arsenic grade cannot meet the international requirement of 99% of arsenic and can only reach 76-92% of crude arsenic. Even the further distillation was also hard to reach the product requirement and involved high cost. (2) Since the smelting temperature was up to 1100-1200°C and materials were under semi-molten state, it was difficult to discharge slag for application in industrial production. (3) The exhaust

issue has not been solved. When arsenic vapor and vapor were generated in the furnace, they would cause the splash of molten materials and produce large quantity of dust polluting the arsenic product and hard to get qualified arsenic. (4) Arsenic content in the slag was up to 10-18%, which brought not only low arsenic recovery, but also the problem of further dearsenization requirement in the subsequent smelting sequence. Another example is some medium and small tests made by means of existing horizontal type horizontal type rotary vacuum furnace to extract element arsenic from arsenopyrite ore, which still has many problems and has not been used for industrial product till now. Main problems are as follows: (1) The arsenic corrosion problem of rotary furnace has not been solved, leading to low furnace life and being not suitable for industrial production. (2) The furnace rotation generates large quantity of dust in the process of continuous stirring of materials, which seriously pollutes the product and is its second fatal weakness. (3) The exhaust problem has not been solved. Under high temperature, vapor generated from crystal water in materials directly enters the vacuum unit, often enables the impossible normal operation of vacuum pump and also leads to failure of vacuum solenoid valve. The requirement on vacuum degree cannot be guaranteed. Sometimes, the water accumulated in the vacuum pump leads to the oxidization of pump parts and rejection of vacuum pump. These accidents happened often lead to leakage of vacuum system and As_2O_3 pollution. (4) Due to continuous rotation of furnace shell, it is very difficult to measure the actual temperature in the rotary body. Plus, such furnace type integrates smelting chamber and crystallization chamber in the same furnace shell. It is more difficult to control temperature at connection between both chambers. (5) Deslagging and product stripping cannot be conducted at the same time. It must first conduct product stripping and then deslagging, which greatly extends the operating time. (6) Since the effective charging size of smelting chamber (material chamber) of

horizontal type rotary furnace is small, and must be less than half the actual size of smelting chamber, otherwise, the materials will flow out of the vent hole (i.e. charging hole) upon rotation and continuously flow into the crystallization chamber and mix with the product. The above problems
5 lead to the fact that the horizontal type rotary vacuum furnace cannot be used for industrial production.

Another example is 100g small tests made by given arsenopyrite ore under vacuum conditions through thermal decomposition and extraction of
10 element arsenic. The test ore charge is pure arsenopyrite ore. Firstly, the mineral is subject to cleaning to remove most impurities, and subject to leaching with the Iron(III) sulfate to remove FeS_2 and other sulfides and get pure arsenopyrite ore as charging material. Although the qualified element arsenic can be got, it is easy to realize for small tests using pure
15 arsenopyrite ore as charging material, and industrial production cannot meet such strict conditions. And the 100g level vacuum furnace has its integrated smelting chamber, crystallization chamber and dust chamber. After furnace shutdown and temperature lowering, the particles of element arsenic are removed from the shell wall (crucible wall). Such tests can
20 only show that the established fact of vacuum thermal decomposition and extraction of element arsenic.

Someone also made tests to adopt minor negative pressure operation in the furnace and enable thermal decomposition of arsenopyrite ore and
25 extraction of element arsenic. So-called minor negative pressure is that the pressure difference between inside and outside the furnace is about 10mm water columns. But the minor negative tests can also only show the established fact of thermal decomposition of arsenopyrite ore and extraction of element arsenic, and cannot eliminate the conditions of
30 generating As_2O_3 , far away from the industrial production.

Contents of Invention

The purpose of this invention is to provide a method of extracting gold from arsenic gold ore concentrate; another purpose of this invention is to provide the system used in the method of extracting gold from arsenic gold ore concentrate.

To overcome the above defects, a method of extracting gold from arsenic gold ore concentrate provided in this invention involves following steps in turn:

- (1) Load the arsenic gold ore concentrate and iron powder into the smelting chamber;
- (2) Increase the temperature of smelting chamber to 100°C-300°C and then hold the temperature to remove the vapor and small quantity of dust in the material;
- (3) Under residual pressure $\leq 50\text{Pa}$, increase the temperature of smelting chamber and crystallization chamber to 300-500°C and then hold the temperature to remove the volatilized arsenic sulfides in the material;
- (4) Hold the temperature of crystallization chamber at 300-500°C, increase the temperature of smelting chamber to 500-600°C and then hold the temperature to remove the gaseous element sulfur decomposed from material;
- (5) Increase the temperature of smelting chamber to 600-760°C and then hold the temperature, meanwhile lower the temperature of crystallization chamber to 270-370°C and then hold the temperature to let the arsenic vapor generated from material to crystallize in the crystallization chamber and get element arsenic and also get gold-rich slag after dearsenization at the bottom of smelting chamber;
- (6) Lower the temperature of smelting chamber and crystallization chamber to below 150°C, charge the air, when the inside and outside

air pressures are basically equal, strip arsenic and draw the gold-rich slag after dearsenization;

(7) Extract fine gold from the gold-rich slag got using conventional method.

Put the arsenic gold ore concentrate material into the crucible. To
5 restrict the discharge of element sulfur causing polluted arsenic
product, add proper quantity of iron powder into the material to fix
sulfur, i.e. $\text{Fe} + \text{S} = \text{FeS}$, let the sulfur stay in the slag by form of FeS,
tighten the mounting nuts 12 of crystallization chamber, start the
induction heating equipment. When the temperature rises to 100-300
10 °C and then hold the temperature, vapor generated in the mineral
along with small quantity of dust gathers into the center
multi-slant-hole collecting and exhaust pipe 9, and connect the vapor
drainage pipe 1 to the exhaust fan, enabling vapor along with small
quantity of dust to drain out of furnace through bottom tightening
15 screw 27 and vapor drainage pipe 1, and ensuring no pollution of
crystallization chamber and vacuum system by vapor and dust. After
the vapor is exhausted, block the vapor drainage outlet and continue
increasing temperature.

20 Using the induction heating equipment to increase temperatures of
smelting chamber and crystallization chamber to 300-500°C and then hold
the temperature, letting arsenic sulfide in material sharply volatilize into
gaseous state (such as As_2S_2 , As_4S_4 , As_2S_3 , etc.) and gather to the center
of collecting and exhaust pipe 9 via its slant hole and continuously flow
25 into the crystallization chamber. Now, since the temperature of
crystallization chamber is about 300-500°C, arsenic sulfide vapor cannot
stay in crystallization chamber due to high vapor pressure, and continue
flowing into the dust chamber, which can be exhausted regularly from the
dust exhaust hole from dust collector and recycled as a byproduct.

Hold the temperature of crystallization chamber at the above 300-500°C, increase the temperature of smelting chamber to 500-600°C and then hold the temperature, to let the FeS₂ decompose a S: FeS₂ =FeS+S (gas), sulfur and iron powder in raw material combine into FeS, and let sulfur stay in the slag by form of FeS.

After the sulfur is completely solidified and various arsenic sulfides are discharged into the dust chamber, continue increasing the temperature of material to 600-760 °C . Material begins sharp decomposition and generates element arsenic vapor:



Now, hold the temperature of smelting chamber at 600-760 °C and crystallization chamber at 270-370 °C . Due to the action of center multi-slant-hole collecting and exhaust pipe 9, arsenic vapor at any point in the material may discharge into the center of exhaust pipe via the nearest slant holes and form continuous arsenic gas flow that flows upward into the constant temperature crystallization chamber, and crystallize on the multi-hole crystallization plate 15 into α arsenic product.

In the whole process of continuous entry of arsenic vapor into the crystallization chamber, the temperature of crystallization chamber must be controlled within 270-370°C. If the temperature is too high, arsenic vapor will flow into dust chamber and no product will be got. If the temperature is too low, β arsenic and γ arsenic will be got, rather than a arsenic product. Since below 760°C , arsenic in the concentrate may completely volatilize, and under such temperature, the low boiling point arsenic and gold compound cannot be generated, thus enabling gold to fully stay in the dry slag.

Shut down, lower temperature and strip product. When material is

completed decomposed without output of arsenic vapor, adopt temperature lowering measures for both interior and exterior shells of crystallization chamber. When the temperature is lowered below 150°C, charge air into the air charging valve 11, till the zero height difference of mercury column of U type pressure gauge, the crystallization chamber can be opened to strip product, draw the gold-rich slag after dearsenization and extract fine gold with the gold-rich slag got by means of conventional method.

10 In the above mentioned method of extracting gold from arsenic gold ore concentrate, before material is charged into the above mentioned smelting chamber, there is a step to crush the arsenic concentrate material into grain size of 0.1mm-2mm.

15 In the above mentioned method of extracting gold from arsenic gold ore concentrate, the weight of above mentioned iron powder is 2-4% of arsenic concentrate material.

20 In the above mentioned method of extracting gold from arsenic gold ore concentrate, holding time is 1-2 hours in the above step (2).

In the above mentioned method of extracting gold from arsenic gold ore concentrate, holding time is 1-2 hours in the above step (3).

25 In the above mentioned method of extracting gold from arsenic gold ore concentrate, holding time is 1-3 hours in the above step (4).

In the above mentioned method of extracting gold from arsenic gold ore concentrate, holding time of smelting chamber and crystallization chamber is respectively 3-7 hours in the above step (5).

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In the above mentioned method of extracting gold from arsenic gold ore concentrate, preferred temperature of smelting chamber in the above step (2) is 200-300°C, and more preferred temperature is 250-300°C.

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In the above mentioned method of extracting gold from arsenic gold ore concentrate, preferred temperature of smelting chamber in the above step (3) is 450-500°C.

10 In the above mentioned method of extracting gold from arsenic gold ore concentrate, preferred temperature of crystallization chamber in the above step (3) is 400-450°C.

15 In the above mentioned method of extracting gold from arsenic gold ore concentrate, preferred temperature of smelting chamber in the above step (4) is 550-600°C.

20 In the above mentioned method of extracting gold from arsenic gold ore concentrate, preferred temperature of crystallization chamber in the above step (4) is 400-450°C.

25 In the above mentioned method of extracting gold from arsenic gold ore concentrate, preferred temperature of smelting chamber in the above step (5) is 650-750°C, and more preferred temperature is 700-750°C.

In the above mentioned method of extracting gold from arsenic gold ore concentrate, the temperature of crystallization chamber in the above step (5) is 300-360°C.

30 This invention provides a kind of system extracting gold from arsenic gold

ore concentrate, including induction heating equipment, smelting device, constant temperature crystallization device, automatic deslagging device, dust collection device, automatic temperature control device, vacuum measuring device and vacuum extraction device. The above mentioned
5 constant temperature crystallization device is fixed on the above mentioned smelting device through demountable device. Its interior smelting chamber is connected with the crystallization chamber of the above mentioned constant temperature crystallization device. Its bottom is connected with the above mentioned automatic deslagging device. The
10 above mentioned smelting device, constant temperature crystallization device and automatic deslagging device have vacuum sealing in between. The above mentioned constant temperature crystallization device is connected with the above mentioned dust collection device through the dust collection inlet pipe. Such dust collection device is connected with the
15 above mentioned vacuum extraction device through pipe equipped with the vacuum measuring device. Inductor on the above mentioned induction heating equipment is arranged on the above mentioned smelting device. The thermal couples 5 of above mentioned automatic temperature control device are respectively mounted on the above mentioned smelting device
20 and constant temperature crystallization device.

In the above mentioned system to extract gold from arsenic gold ore concentrate, the above mentioned smelting device consists of: crucible formed by detachable bottom 8', cover 26 and wall 8, vacuum furnace
25 shell 7 assembled outside the crucible, as well as a hollow collecting and exhaust pipe 9 vertically mounted at the center of the above mentioned crucible bottom 8'. The interior wall of the above mentioned crucible and exterior wall of the above mentioned collecting and exhaust pipe 9 form the above mentioned smelting chamber, which connects with the above
30 mentioned crystallization chamber through the top of the above mentioned

collecting and exhaust pipe 9. Many downward slant holes are distributed on the wall of such collecting and exhaust pipe 9. A vapor drainage pipe 1 is also installed under such collecting and exhaust pipe 9, which crosses the above mentioned crucible bottom 8' and connects with an exhaust fan.

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In the above mentioned system to extract gold from arsenic gold ore concentrate, the centerline of each slant hole of the above mentioned collecting and exhaust pipe 9 and the centerline of the above mentioned collecting and exhaust pipe 9 are in the same plane and form 20-40 degree bevel with the lower end face of the above mentioned collecting and exhaust pipe 9.

In the above mentioned system to extract gold from arsenic gold ore concentrate, the above mentioned crucible is made of corrosion proof and heat conducting material, preferably made of graphite.

In the above mentioned system to extract gold from arsenic gold ore concentrate, the inductor of the above mentioned induction heating equipment is of intermediate frequency inductor. Such intermediate frequency inductor is in integral cast in the insulating materials and assembled in the vacuum furnace shell 7 outside the above mentioned crucible. The above mentioned induction heating equipment also includes intermediate frequency power, capacitor for electric induction heating system, intermediate frequency isolating transformer. The above mentioned intermediate frequency isolating transformer is connected between the electric input end of the above mentioned intermediate frequency inductor and intermediate frequency power.

In the above mentioned system to extract gold from arsenic gold ore concentrate, the inductor of the above mentioned induction heating

equipment is of intermediate frequency inductor. Such inductor is assembled outside the above mentioned vacuum furnace shell 7. The above mentioned induction heating equipment also includes intermediate frequency power and capacitor for electric induction heating system.

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In the above mentioned system to extract gold from arsenic gold ore concentrate, the above mentioned vacuum furnace shell 7 is made of high temperature resistant, insulation, non-magnetoconductive, non conducting and non-leakage material, preferably made of ceramic or 4-fluorothene plastic wire mesh.

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In the above mentioned system to extract gold from arsenic gold ore concentrate, insulating material is used to block the gap between the above mentioned crucible wall 8 and the above mentioned vacuum furnace shell 7.

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In the above mentioned system to extract gold from arsenic gold ore concentrate, the above mentioned constant temperature crystallization device includes bottomless shell 14 and inner shell 13, many multi-hole crystallization plates 15 installed on one support as well as center heating pipe 16 installed on the above mentioned shell 14 and extending at the vertical direction in the center of shell. The space in the above mentioned inner shell 13 forms the above mentioned crystallization chamber. The above mentioned inner shell 13 and support of multi-hole crystallization plate 15 are fixed together with the above mentioned shell 14 through the dismountable device.

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In the above mentioned system to extract gold from arsenic gold ore concentrate, a minor annular slit exists between the shell 14 and inner shell 13 of the above mentioned constant temperature crystallization

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device. The bottom of the above mentioned annular slit is plugged with refractory materials.

In the above mentioned system to extract gold from arsenic gold ore concentrate, the above mentioned automatic temperature control device includes: a thermal couple 5 inserted on the crystallization chamber shell 14 for measuring temperature in the crystallization chamber, a thermal couples 5 inserted at the furnace bottom 6 for measuring temperature of smelting chamber, as well as temperature controller connected with the above two thermal couples 5 and the above mentioned induction heating equipment through compensation cord for respectively controlling the temperature in the furnace and crystallization chamber.

In the above mentioned system to extract gold from arsenic gold ore concentrate, the above mentioned smelting device is installed above the ground through the support 24. Such smelting device also includes a furnace bottom 6 fixed with the above mentioned crucible bottom 8'; the above mentioned automatic deslagging device includes: hopper 4, slag car 3 as well as hydraulic lift 2 installed on the hopper 4. The above mentioned furnace bottom 6 is connected with vacuum furnace shell 7 through top support of the hydraulic lift 2, between which the vacuum sealing strips are used for vacuum sealing. Upon lowering, such hydraulic lift 2 can separate the above mentioned furnace bottom 6 and the above mentioned crucible bottom 8' from the above mentioned crucible wall 8.

In the above mentioned system to extract gold from arsenic gold ore concentrate, a layer of heat insulation material is arranged between the above mentioned crucible bottom 8' and the above mentioned furnace bottom 6.

Brief Description of the Drawings

Fig.1 is the flow diagram of the method of extracting gold from arsenic gold ore concentrate provided in this invention.

5 Fig.2 is one structural representation of the system of extracting gold from arsenic gold ore concentrate provided in this invention.

Fig.3 is another structural representation of the system of extracting gold from arsenic gold ore concentrate provided in this invention.

10 Detailed Embodiments

Now, further explanations on the method of extracting gold from arsenic gold ore concentrate provided in this invention and the system of extracting gold from arsenic gold ore concentrate provided in this
15 invention are given in combination with the drawings.

Please refer to one structural representation of the system of extracting gold from arsenic gold ore concentrate provided shown in Fig.2, brief explanations on structural features and operating principle of major
20 equipment in this invention are made.

In the system of extracting gold from arsenic gold ore concentrate provided in this invention, smelting device is connected with the constant temperature crystallization device through bolts and nuts, between which
25 the rubber strip is used for vacuum sealing; smelting device is connected with the automatic deslagging device with hydraulic operated furnace bottom through hydraulic lift 2; the constant temperature crystallization device is connected with the dust collection device through left flange of dust collection inlet pipe 17. "O" rubber ring is used between left and right
30 flanges for vacuum sealing; the dust collection device is connected with

the vacuum extraction device through stainless steel pipe and solenoid valve 23; the intermediate frequency induction heating equipment is connected with the smelting device through the inductor 10; inductor 10 and intermediate frequency heating device are connected through flexible cable; the temperature controlling device is connected with all temperature control instruments through thermal couples 5 and compensation flexible conductor. Thyristor is controlled through information feedback of thermal couples 5 to automatically adjust power and control temperature; the pressure measuring device is connected with the macleod gauge and U type pressure gauge with vacuum hose and pressure sensing tube connector 20 to read the vacuum degree.

Intermediate frequency heating part 10 is put in stainless steel vacuum furnace shell 7 on the vacuum furnace support 24. To prevent vacuum discharge, on the one hand, the whole intermediate frequency inductor must be cast and sealed with insulating material to prevent inductor shorted to earth. On the other hand, the intermediate frequency isolating transformer is connected between the electric input end of the intermediate frequency inductor and intermediate frequency power to lower the intermediate frequency output voltage and further prevent the vacuum discharge in the furnace.

A hollow collecting and exhaust pipe 9 is vertically installed at the center of graphite crucible bottom 8'. Its top is connected with the constant temperature crystallization device and enables the fixed connection between multi-slant-hole collecting and exhaust pipe 9 and graphite crucible bottom 8'. Upward slant holes are evenly distributed on the collecting and exhaust pipe. Each slant hole forms 30 degree bevel with the lower end face of collecting and exhaust pipe. The role of these slant holes is to enable various gases generated by materials in the furnace to

gather to the center of collecting and exhaust pipe in the shortest distance and minimum flow resistance, enter the multi-hole crystallization plate 15 of constant temperature crystallization chamber from the collecting and exhaust pipe, and crystallize into the arsenic product. The center
5 collecting and exhaust pipe can greatly reduce the flow resistance of various gases generated by the melted materials, such as arsenic vapor, steam, various arsenic sulfide vapors and so on, and also minimize the arsenic content in the slag. A vapor drainage pipe 1 is under such collecting and exhaust pipe 9, crosses the above mentioned graphite
10 crucible bottom 8' and connects with the exhaust fan.

The automatic deslagging device with hydraulic operated furnace bottom includes slag car 3, slag hopper 4, hydraulic lift 2 and lifting furnace bottom 6. Such lifting furnace bottom 6 is fixed with the graphite crucible
15 bottom 8' through insulating material layer. The furnace bottom 6 is connected with the stainless steel vacuum furnace shell 7 through the support of hydraulic lift 2, between which the vacuum rubber strips are used for vacuum sealing. The hydraulic lift 2 drives the furnace bottom 6 and graphite crucible bottom 8' to separate from the above mentioned
20 graphite crucible wall 8. The hydraulic lift 2 upward supports such furnace bottom 6 to compact the vacuum rubber strips between such furnace bottom 6 and stainless steel vacuum furnace shell 7 and fulfill vacuum sealing. The lifting of furnace bottom arrives at the purpose of automatic deslagging. The reason why deslagging by means of lifting the furnace
25 bottom is because the smelting temperature $\leq 760^{\circ}\text{C}$, any substances in the material are far from the melting conditions and the slag is dry and of the same flow property with the original material.

Center heating pipe 16 extending in vertical direction is installed at the
30 center of constant temperature crystallization chamber, on the

crystallization chamber shell 14 and shell center. Several equidistant multi-hole crystallization plates 15 are installed at one tubular support. Such tubular support is also assembled outside the above mentioned center heating pipe 16. The crystallization chamber inner shell 13 and multi-hole crystallization plate 15 are fixed with the crystallization chamber external shell 14 through bolts and nuts 12. Screwing off the nut 12 can take off all multi-hole crystallization plates and crystallization chamber inner shell so as to strip product. There is a minor annular slit between such crystallization chamber inner shell 13 and external shell 14 to facilitate removing the crystallization chamber inner shell 13. Since arsenic vapor is not allowed to enter such slit for crystallization, otherwise, it will cause the accident of blocking the inner shell 13. To prevent such accident, the spongy refractory materials shall be properly plugged into the lower end of such annular slit.

The temperature control of smelting chamber is fulfilled by means of thermal couples 5 installed at the lifting furnace bottom 6 for information feedback to the temperature controlling device on the intermediate frequency induction heating equipment. And the thyristor in the temperature controlling device can automatically adjust the intermediate frequency voltage in the thyristor according to the feedback information, i.e. adjusting the output power of intermediate frequency to arrive at the purpose of temperature control. The constant temperature crystallization chamber has dedicated and independent temperature controlling device for temperature control. Its temperature control principle is the same as that of smelting chamber, using thermal couples 5 installed at the crystallization chamber external shell 14 for information feedback. The temperature controlling device automatically adjusts the heating power of electric furnace heating wires wound on the center heating pipe 16 according to the changing information to arrive at the purpose of

temperature control of crystallization chamber. The electric furnace heating wires on the heating pipe must be completely isolated with the arsenic vapor from arsenic corrosion. The above mentioned tubular support plays the role of isolating the arsenic vapor from entry into the center heating chamber.

The constant temperature crystallization chamber external shell 14 is connected with the dust collector shell 18 through the dust collection inlet pipe 17. When the temperature rises to 300--500℃, various arsenic sulfides volatilized from materials enter the dust chamber and are discharged through dust exhaust hole as byproducts.

The top of dust chamber 18 is connected into the vacuum extraction system with the stainless steel extraction pipe. By starting the vacuum unit 22, the whole integrated system arrives at the vacuum requirement through vacuum solenoid valve 23 and stainless steel extraction pipe. The air charging valve 21 can be used to carry out system charging leakage check. The system vacuum degree can be measured by use of U type pressure gauge and macleod gauge connected on the pressure measuring pipe 20.

Please refer to another structural representation of the system of extracting gold from arsenic gold ore concentrate provided shown in Fig.3, brief explanations on another structural features and operating principle of smelting device are given below. The installation descriptions of other devices are the same as those of Fig.2.

It is put inside the ceramic vacuum furnace shell 7 on the vacuum furnace support 24 and fixed with screw 13 and furnace shell fixing screw 17. Since the tailor-made industrial ceramic furnace shell can not only meet

the requirement of no leakage under high vacuum, but also meet the special non-magnetoconductive, non conducting, high temperature resistant and high strength requirement required by electric magnetic induction heating, it is allowed to assemble the inductor 10 outside the industrial ceramic furnace shell 7. Such structure can completely eliminate the phenomenon of vacuum discharge, improve the operating reliability of heating system, and also get rid of the intermediate frequency isolating transformer required by conventional vacuum furnace for preventing the vacuum discharge and save the power consumption of isolating transformer. More significantly: in case the stainless steel is used as the vacuum furnace shell, it has to put the inductor inside the stainless steel shell, leading to magnetic induction heating of stainless steel shell and adding useless power consumption. This invention adopts tailor-made ceramic vacuum furnace shell, whose total power consumption may be saved by 20-30% under the same power.

The graphite crucible wall 8, graphite crucible bottom 8' and graphite crucible cover 26 are installed in the ceramic vacuum furnace shell 7. A hollow collecting and exhaust pipe 9 is vertically installed at the center of graphite crucible bottom 8'. Annular slit between ceramic shell and graphite crucible is plugged with insulating material 4.

Taking the arsenic sulfide gold ore concentrate as material, further descriptions on this method are made through following experimental data:

Table [1] Influence of Grain Size of Arsenic Sulfide Gold Ore Concentrate on Arsenic Volatilization Amount

Arsenic volatilization amount	kg	650	740	796	848
	%	<75%	<85%	≤91%	97%

Grain size (mm)	5—10	3—5	1—3	0.1—2
Temperature (°C)	750			
Residual pressure (Pa)	1—50			
Charge (kg)	2500			
Distillation time (h)	4			
Concentrate arsenic grade (%)	35			

It is seen from Table [1] that in the event of unchanged 5 conditions like temperature and residual pressure, when the grain size is 0.1-2mm, the optimum distillation effect can be got.

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To show the relation between arsenic sulfide volatilization rate and temperature, we made a test by the mini vacuum furnace. The test result is listed in Table [2].

10 Table [2] Influence of Temperature on Arsenic Sulfide Volatilization Rate

Arsenic sulfide volatilization amount	g	1	5	9.5	9.8
	%	10%	50%	95%	100%
Temperature (°C)		300	400	450	500
Grain size (mm):		0.1—2			
Residual pressure (Pa)		50			
Charge (g)		100			
Distillation time (min)		30			
Arsenical sulfide grade (%)		10			

It is seen from Table [2] that when the temperature is at 450°C, within 30 minutes, 95% arsenic sulfides have been volatilized. If time is extended further, 100% will be volatilized. So, 450-500 °C is the optimum decomposition temperature of arsenic sulfides.

5 To show the relation between FeS₂ decomposition and temperature, the mini vacuum furnace is also used to make a test. The test result is listed in the Table [3].

10 Table [3] Relation Between FeS₂ Decomposition and Temperature

Separated sulfur amount	g	0	0.53	4.24	5.2	5.3
	%	0	10%	80%	98%	100%
Temperature (°C)		300	450	500	550	600
Grain size (mm)		0.1-2				
Residual pressure (Pa)		50				
Charge (g)		100				
Distillation time (h)		1				
FeS grade (%)		20				

15 It is seen from Table [3] that when the temperature is 550°C, large amount of FeS₂ may be decomposed: FeS₂=FeS+S (gas), up to 98% at such temperature. If time is extended further, 100% will be decomposed. So, 550-600°C is the optimum decomposition temperature of FeS₂.

Table [4] Influence of Temperature on Arsenic Volatilization Amount

Arsenic volatilization amount	Kg	175	350	700	860
	%	20%	40%	80%	>98%
Temperature (°C)		550-600	600-650	650-700	700-750
Grain size (mm)		0.1—2			
Residual pressure (Pa)		1—50			
Charge (g)		2500			
Distillation time (h)		4			
Concentrate arsenic grade (%)		35			

- 5 It is seen from Table [4] that in the event of unchanged 5 conditions like grain size and residual pressure, when the temperature is 650-700°C, the arsenic volatilization is up to 80%; when the temperature is 700-750°C, the arsenic volatilization is up to the maximum amount. The slag now is still of dry slag without caking and melting. It keeps the good flow property with
10 the original material. Apparently, if the distillation time is extended further, the volatilization amount will increase.

Embodiment 1:

- Please refer to Fig.1 the flow diagram of the method of extracting gold
15 from arsenic gold ore concentrate provided in this invention. Crush 2.5t arsenic sulfide gold ore concentrate into 1mm grain size and put the same into the graphite crucible. Add 62kg scrap iron powder to fix sulfur and enable it to stay in the slag by form of FeS. Tighten the crystallization chamber mounting nut 12. Start the intermediate frequency heating device.

Experimental conditions are shown as Table [5]. Increase the temperature to 100°C and then hold the temperature for 2 hours to remove the vapor and small quantity of dust in the arsenic sulfide gold ore concentrate. Vapor along with small quantity of dust generated from the concentrate gather into the center multi-slant-hole collecting and exhaust pipe 9. Connect the vapor drainage pipe 1 to the exhaust fan to discharge vapor and small quantity of dust through furnace bottom tightening screw 27 and vapor drainage pipe 1. When the vapor is drain out, block the vapor drainage hole; continue increasing the temperature to remove the volatilized arsenic sulfides in the arsenic sulfide gold ore concentrate, and when the temperature of smelting chamber and crystallization chamber rises to 300°C and then hold the temperature for 2 hours, letting arsenic sulfides in concentrate volatilize into gaseous state (such as As_2S_2 , As_4S_4 , As_2S_3 , etc.) and gather to the center of collecting and exhaust pipe 9 via the slant holes of collecting and exhaust pipe, flow into the crystallization chamber, then to the dust chamber; to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, hold the crystallization chamber temperature at 300 °C , use the intermediate frequency heating device to increase the smelting chamber temperature to 500°C and then hold the temperature for 2 hours. The decomposed element sulfur combines with scrap iron powder in the raw material into FeS, letting the element sulfur stay in the slag by form of FeS; to get element arsenic in the arsenic sulfide gold ore concentrate, continue increasing smelting chamber temperature to 600°C and then hold the temperature for 7 hours, lower the crystallization chamber temperature to 270°C and then hold the temperature for 7 hours. Generated element arsenic vapor is drained into the center of collecting and exhaust pipe from the nearest slant hole to form arsenic gas flow, which continuously flows into the constant temperature crystallization chamber and crystallize on multi-hole crystallization plate 15 into α arsenic product.

Adopt temperature lowering measures for both interior and exterior shells of smelting chamber and crystallization chamber. When the temperature is lowered below 150°C, charge air into the air charging valve 11, till the zero height difference of mercury column of U type pressure gauge, the crystallization chamber can be opened to strip product, take out the gold-rich slag after dearsenization. The experimental result is shown as Table[5]. The purity of arsenic product is 80% and concentrate dearsenization rate is 50%.

The known thiourea or cyanidation is used to treat the gold-rich slag after dearsenization and extract gold. The gold recovery is up to 90%-95%.

Embodiment 2:

The same experimental steps as Embodiment 1 are adopted. The difference lies in that to remove the vapor and small quantity of dust in the arsenic sulfide gold ore concentrate, increase the temperature to 150°C and then hold the temperature for 2 hours; to remove the volatilized arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the temperature of smelting chamber and crystallization chamber to 320°C and then hold the temperature for 2 hours; to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 300 °C , and increase the smelting chamber temperature to 530°C and then hold the temperature for 2 hours; to get the element arsenic in the arsenic sulfide gold ore concentrate, hold the crystallization chamber at 300 °C for 7 hours, continue increasing the smelting chamber temperature to 630°C and then hold the temperature for 7 hours. α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table[5]. The purity of arsenic product is 82% and concentrate

dearsenization rate is 55%.

Embodiment 3:

The same experimental steps as Embodiment 1 are adopted. The
5 difference lies in that to remove the vapor and small quantity of dust in the
arsenic sulfide gold ore concentrate, increase the temperature to 200°C
and then hold the temperature for 1.5 hours; to remove the volatilized
arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the
temperature of smelting chamber to 350°C, and increase the temperature
10 of crystallization chamber to 300°C, and then hold the temperature for 1.5
hours; to remove the decomposed gaseous element sulfur in the arsenic
sulfide gold ore concentrate, increase the crystallization chamber
temperature to 320°C, increase the temperature of smelting chamber to
570°C and then hold the temperature for 1.5 hours; to get the element
15 arsenic in the arsenic sulfide gold ore concentrate, lower the crystallization
chamber temperature to 300°C and then hold the temperature for 6 hours,
continue increasing the smelting chamber temperature to 650°C and then
hold the temperature for 6 hours. α arsenic product is crystallized on the
multi-hole crystallization plate 15. The experimental result is shown as
20 Table[5]. The purity of arsenic product is 85% and concentrate
dearsenization rate is 60%.

Embodiment 4:

The same experimental steps as Embodiment 1 are adopted. The
25 difference lies in that to remove the vapor and small quantity of dust in the
arsenic sulfide gold ore concentrate, increase the temperature to 200°C
and then hold the temperature for 1.5 hours; to remove the volatilized
arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the
temperature of smelting chamber to 400°C, and increase the temperature
30 of crystallization chamber to 350°C, and then hold the temperature for 1.5

hours; to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, increase the crystallization chamber temperature to 400°C, increase the temperature of smelting chamber to 600°C and then hold the temperature for 1.5 hours; To get the element arsenic in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 320°C and then hold the temperature for 6 hours, continue increasing the smelting chamber temperature to 670°C and then hold the temperature for 6 hours. α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table[5]. The purity of arsenic product is 97% and concentrate dearsenization rate is 70%.

Embodiment 5:

The same experimental steps as Embodiment 1 are adopted. The difference lies in that to remove the vapor and small quantity of dust in the arsenic sulfide gold ore concentrate, increase the temperature to 230°C and then hold the temperature for 1.3 hours; to remove the volatilized arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the smelting chamber temperature to 400°C, and increase the temperature of crystallization chamber to 300°C, and then hold the temperature for 1.5 hours; to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, hold the crystallization chamber temperature at 300°C, increase the smelting chamber temperature to 570°C and then hold the temperature for 2 hours; to get the element arsenic in the arsenic sulfide gold ore concentrate, hold the crystallization chamber temperature at 300 °C for 6 hours, continue increasing the smelting chamber temperature to 680°C and then hold the temperature for 6 hours. α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table [5]. The purity of arsenic product is 86% and concentrate dearsenization rate is 80%.

Embodiment 6:

The same experimental steps as Embodiment 1 are adopted. The difference lies in that to remove the vapor and small quantity of dust in the arsenic sulfide gold ore concentrate, increase the temperature to 230°C and then hold the temperature for 1 hour; to remove the volatilized arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the smelting chamber temperature to 450 °C , and increase the temperature of crystallization chamber to 400°C, and then hold the temperature for 1 hour; to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, hold the crystallization chamber temperature at 400 °C, increase the smelting chamber temperature to 600°C and then hold the temperature for 1 hour; to get the element arsenic in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 350°C and then hold the temperature for 5 hours, continue increasing the smelting chamber temperature to 700°C and then hold the temperature for 5 hours. α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table [5]. The purity of arsenic product is 99% and concentrate dearsenization rate is 90%.

Embodiment 7:

The same experimental steps as Embodiment 1 are adopted. The difference lies in that to remove the vapor and small quantity of dust in the arsenic sulfide gold ore concentrate, increase the temperature to 230°C and then hold the temperature for 1.3 hours; to remove the volatilized arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the smelting chamber temperature to 450°C , and increase the temperature of crystallization chamber to 330°C, and then hold the temperature for 1 hour;

to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, increase the crystallization chamber temperature to 450°C, increase the smelting chamber temperature to 550°C and then hold the temperature for 2.5 hours; to get the element arsenic in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 320°C and then hold the temperature for 4.5 hours, continue increasing the smelting chamber temperature to 730°C and then hold the temperature for 4.5 hours. α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table[5]. The purity of arsenic product is 99% and concentrate dearsenization rate is 94%.

Embodiment 8:

The same experimental steps as Embodiment 1 are adopted. The difference lies in that to remove the vapor and small quantity of dust in the arsenic sulfide gold ore concentrate, increase the temperature to 250°C and then hold the temperature for 1 hour; to remove the volatilized arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the smelting chamber temperature to 500 °C , and increase the temperature of crystallization chamber to 430°C, and then hold the temperature for 1 hour; to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 400 °C, increase the smelting chamber temperature to 620°C and then hold the temperature for 1 hour; to get the element arsenic in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 350°C and then hold the temperature for 5 hours, continue increasing the smelting chamber temperature to 730°C and then hold the temperature for 6 hours. α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table [5]. The purity of arsenic product is 99% and concentrate dearsenization rate is

97%.

Embodiment 9:

The same experimental steps as Embodiment 1 are adopted. The
5 difference lies in that to remove the vapor and small quantity of dust in the
arsenic sulfide gold ore concentrate, increase the temperature to 280°C
and then hold the temperature for 1 hour; to remove the volatilized arsenic
sulfides in the arsenic sulfide gold ore concentrate, increase the smelting
chamber temperature to 480 °C , and increase the temperature of
10 crystallization chamber to 450°C; and then hold the temperature for 1 hour;
to remove the decomposed gaseous element sulfur in the arsenic sulfide
gold ore concentrate, lower the crystallization chamber temperature to 430
°C, increase the smelting chamber temperature to 620°C and then hold
the temperature for 1 hour; to get the element arsenic in the arsenic
15 sulfide gold ore concentrate, lower the crystallization chamber
temperature to 320°C and then hold the temperature for 3 hours, continue
increasing the smelting chamber temperature to 750°C and then hold the
temperature for 3 hours. α arsenic product is crystallized on the multi-hole
crystallization plate 15. The experimental result is shown as Table [5]. The
20 purity of arsenic product is 99% and concentrate dearsenization rate is
98%.

Embodiment 10:

The same experimental steps as Embodiment 1 are adopted. The
25 difference lies in that to remove the vapor and small quantity of dust in the
arsenic sulfide gold ore concentrate, increase the temperature to 300°C
and then hold the temperature for 1 hour; to remove the volatilized arsenic
sulfides in the arsenic sulfide gold ore concentrate, increase the smelting
chamber temperature to 500 °C , and increase the temperature of
30 crystallization chamber to 450°C, and then hold the temperature for 1 hour;

to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, hold the crystallization chamber temperature at 450 °C, increase the smelting chamber temperature to 620°C and then hold the temperature for 1 hour; to get the element arsenic in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 340°C and then hold the temperature for 3 hours, continue increasing the smelting chamber temperature to 760°C and then hold the temperature for 3 hours, α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table [5]. The purity of arsenic product is 99% and concentrate dearsenization rate is 98%.

Embodiment 11:

The same experimental steps as Embodiment 1 are adopted. The difference lies in that to remove the vapor and small quantity of dust in the arsenic sulfide gold ore concentrate, increase the temperature to 300°C and then hold the temperature for 1 hour; to remove the volatilized arsenic sulfides in the arsenic sulfide gold ore concentrate, increase the smelting chamber temperature to 480 °C , and increase the temperature of crystallization chamber to 350°C, and then hold the temperature for 1 hour; to remove the decomposed gaseous element sulfur in the arsenic sulfide gold ore concentrate, increase the crystallization chamber temperature to 420°C, increase the smelting chamber temperature to 580°C and then hold the temperature for 1.8 hours; to get the element arsenic in the arsenic sulfide gold ore concentrate, lower the crystallization chamber temperature to 350°C and then hold the temperature for 3 hours, continue increasing the smelting chamber temperature to 750°C and then hold the temperature for 3.5 hours. α arsenic product is crystallized on the multi-hole crystallization plate 15. The experimental result is shown as Table[5]. The purity of arsenic product is 99% and concentrate

dearsenization rate is 98%.

Industrial Practicability

This invention provides a method of extracting gold from arsenic gold ore concentrate, where the atmosphere doesn't attend the chemical reaction of materials in the furnace under vacuum condition, thus radically eliminating the condition generating virulent As_2O_3 , and also radically eliminating the condition generating waste gas and wastewater, which is a breakthrough of gold smelting environment protection technology. To extract arsenic under residual pressure $\leq 50\text{Pa}$ and temperature 760°C is not possible to generate the low boiling point arsenic and gold compound. Therefore, the whole dearsenization process has no gold volatilization loss, which effectively solves the problem of low recovery of fine grained and submicron. Through large-scale production experiments, this invention fulfills its purpose and anticipated effect.

The crucible on the smelting chamber wall in the system of extracting gold from arsenic gold ore concentrate provided in this invention is made of corrosion resistant and heat conducting material, solving the problem of corrosion and low furnace life of existing horizontal type rotary vacuum furnace; since this vacuum smelting device is fixed through support, avoiding the fatal weakness of seriously polluting product due to large quantity of dust generated by material in furnace rotation, and the temperature is easily measured; a vapor drainage pipe 1 connected with the exhaust fan under the collecting and exhaust pipe 9 in the smelting chamber of this vacuum smelting device is installed, avoiding the problems of direct entry of steam generated from crystal water in materials under high temperature into the vacuum unit, which enables the impossible normal operation of vacuum pump and also the failure of vacuum solenoid valve and being unable to guarantee the requirement on

vacuum degree, and sometimes, the water accumulated in the vacuum pump leads to the oxidization of pump parts and rejection of vacuum pump; since the system respectively is equipped with smelting device, constant temperature crystallization device, automatic deslagging device and dust collection device, pure product can be got, enabling easy temperature control of the smelting chamber and crystallization chamber and simultaneous deslagging and product stripping; since this system adopts the vertical structure, thus enlarging the effective charging size of smelting chamber. This system overcomes existing problems of horizontal type rotary vacuum furnace and is suitable for industrial production. It features three functions: (1) being able to completely decompose arsenic in the arsenic gold ore concentrate under low temperature and get the international standard element arsenic product. (2) enabling element sulfur decomposed from the arsenic gold ore concentrate and various arsenic sulfides volatilized to gather in the dust chamber where such byproduct is got. (3) The whole process of gold extraction has no discharge of wastewater, waste gas and toxic slag.

Table[5]

Embodiment	Steam drainage and dust exhaust temperature (°C)	Holding time (h)	Volatile arsenic sulfide temperature(°C)		Holding time (h)	Sulfur decomposition Temperature (°C)		Holding time (h)	Temperature of smelting chamber generating arsenic vapor (°C)	Holding time (h)	Temperature of crystallization chamber for arsenic crystallization (°C)	Holding time (h)	Arsenic purity (As%)	Dearsenization rate (%)
			Smelting chamber	Crystallization chamber		Smelting chamber	Crystallization chamber							
1	100	2	300	300	2	500	300	2	600	7	270	7	80	50
2	150	2	320	320	2	530	300	2	630	7	300	7	82	55
3	200	1.5	350	300	1.5	570	320	1.5	650	6	300	6	85	60
4	200	1.5	400	350	1.5	600	400	1.5	670	6	320	6	97	70
5	230	1.3	400	300	1.5	570	300	2	680	6	300	6	86	80
6	230	1	450	400	1	600	400	1	700	5	350	5	99	90
7	230	1.3	450	330	1	550	450	2.5	730	4.5	320	4.5	99	94
8	250	1	500	430	1	620	400	1	730	5	350	5	99	97
9	280	1	480	450	1	620	430	1	750	3	320	3	99	98
10	300	1	500	450	1	620	450	1	760	3	340	3	99	98
11	300	1	480	350	1	580	420	1.8	750	3.5	350	3.5	99	98